



TU1406

COST ACTION

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QUALITY SPECIFICATIONS FOR ROADWAY BRIDGES,
STANDARDIZATION AT A EUROPEAN LEVEL

TU1406 WG4 Final report

Appendix A14

Bridge Case study

**Girder bridge – Güney Yaklaşım Viyadüğü
(South Approach Viaduct),**

Altınova, TURKEY

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1. GENERAL DATA OF THE BRIDGE

1.1. BRIDGE LOCATION

South Approach Viaduct is 1,378 meters long and located at south of Osmangazi Bridge in TURKEY. Areal map of the bridge location is presented below:



Figure 1: Bridge location

1.2. TRAFFIC INFORMATION

Number of cars / 30 days in Bursa direction : 275,561.-

Number of cars / 30 days in İstanbul direction : 286,896.-

Heavy Vehicles : %5

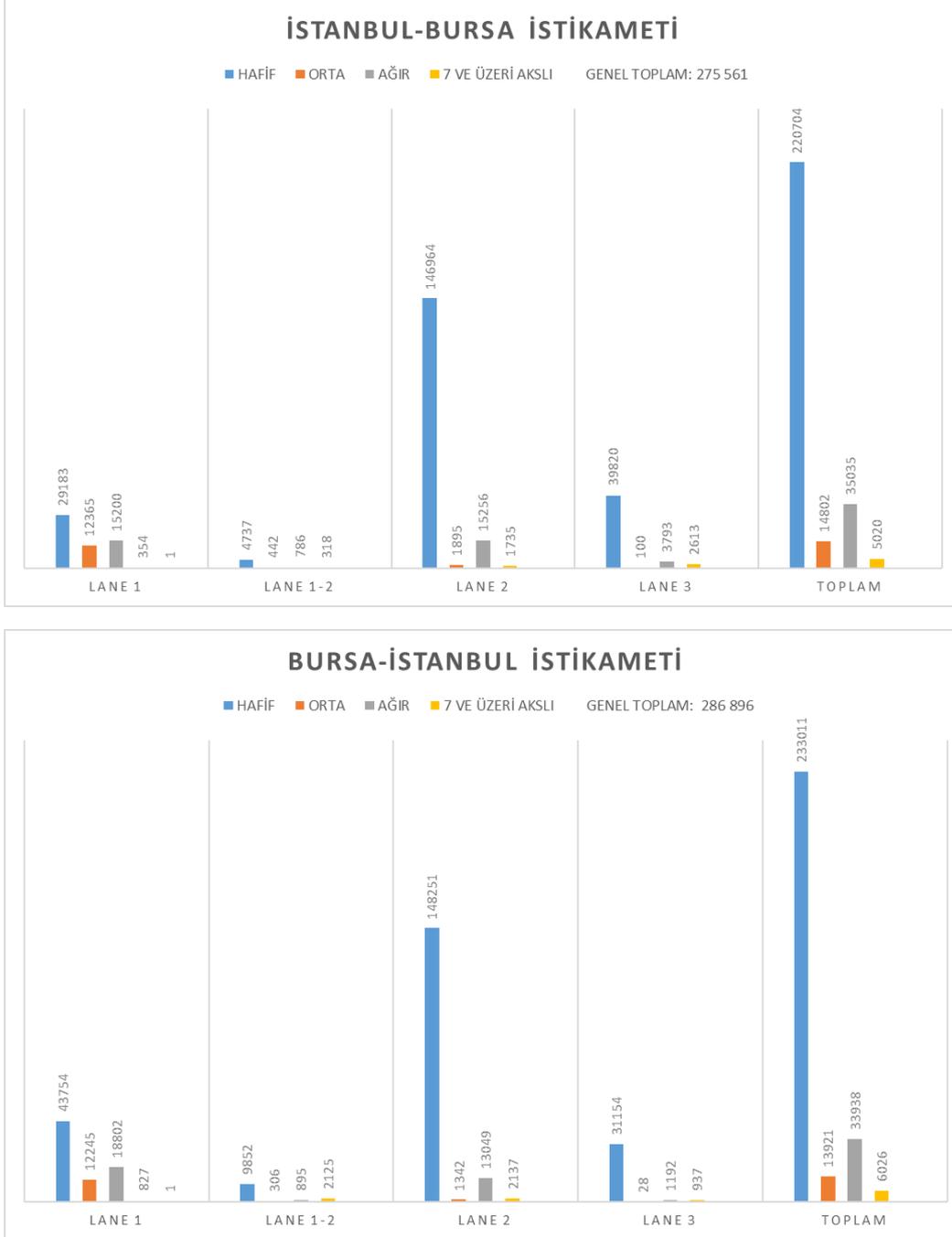


Figure 2: Number of cars from WIM report

1.3. PLAN AND CROSS-SECTION OF BRIDGE

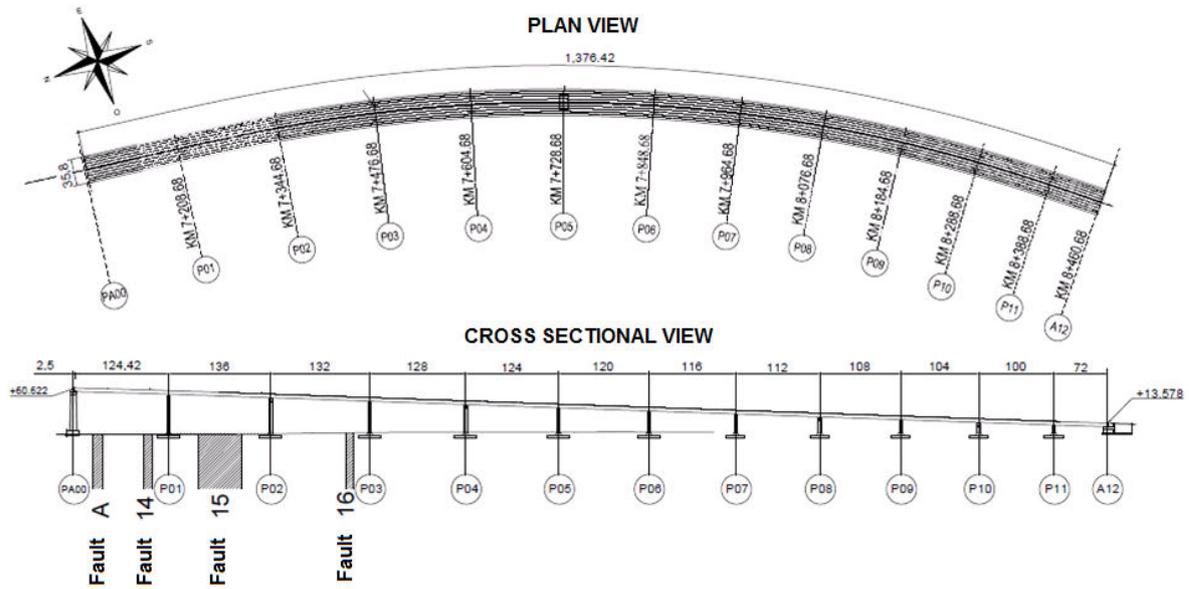


Figure 3: Bridge plan and longitudinal cross-section

1.4. SEISMICITY OF AREA

South Approach Viaduct is constructed in one of the most seismically active places in the world. The bridge connects the Diliskelesi peninsula to the North with the Hersek peninsula on the south. The proposed project site spans the plate boundary between the Anatolian plate on the south and the Eurasian plate on the north and will experience significant earthquakes on the North Anatolian Fault Zone (source of the 1999 Magnitude Mw 7.4 Izmit and Mw 7.2 Düzce earthquakes).

1.5. BRIDGE PROPERTIES

The South Approach Viaduct of the Osmangazi Bridge Crossing brings the bridge down from on the order of elevation 60 meters at the South Anchorage to an elevated embankment approximately 1378 meters further south. The bridge consists of 11 Piers and 10 standard intermediate spans with lengths varying between 136 m and 100 m and two bank spans one of 125 m, attached to the main bridge and the other of 72 m attached to the south embankment (Figure 4). The South Approach Viaduct is located between km 7+084.26 (Pier P0) and km 8+462.43 (Pier A12). The SAV piers are numbered consecutively starting from Pier P1 which is located south of the South Anchorage of the main Bridge to Pier P11 and terminating at the south embankment A12, located south of Pier P11. The interface between the Osmangazi Bridge and the SAV is at the South Anchorage of the Osmangazi Bridge (Pier P0).



Figure 4: General layout of footings

1.6. SUBSOIL AND GEOLOGY

Prior to the construction of the foundations, a detailed geophysical and geotechnical survey program was executed between 2011 and 2012. The site investigation consisted of 10 no. of boreholes down to 60 m depth; 126 no. of Menard Pressuremeter tests in all boreholes; 48 no. of CPT; and laboratory tests. Since the site is underlain by deep deposits of soft soils, and areas of unstable and liquefiable soils, characterizing the geological, seismological and geotechnical setting, foundation soil conditions, fault locations, as well as developing an appropriate design criteria was the most critical component for the project.

1.7. FOUNDATION CONCEPT

Analyses were performed to evaluate the performance of two different foundation types for the SAV piers, a shallow foundation and a diaphragm wall foundation system. Due to the severity of the design ground motions, the superstructure introduces significant moments on the foundation. For a shallow footing solution, the size of the

footing is driven by the overturning resistance to the superstructure loads rather than the vertical bearing capacity. Additionally, since fault rupture through a pier foundation is the main concern for this project, the foundation system was found to play a key role in the response of structures subjected to fault induced ground movement. Structures resting on rigid and continuous foundation systems (such as a raft, or a box-type foundation) have demonstrated to be capable of achieving a very satisfactory performance, irrespective of the faulting type. As a result; a caisson-type of foundation was selected as the most suitable foundation system; which consists of four perimeter diaphragm walls, a concrete cap, and a diaphragm wall constructed along the bridge transverse direction under each Pier legs. The thickness of the diaphragm walls is 1.00 meter and the cap thickness is 3 meters. The foundation concept is shown schematically in Figure 5. A total of 14,400 m² diaphragm wall with a maximum depth of 23 m was executed.

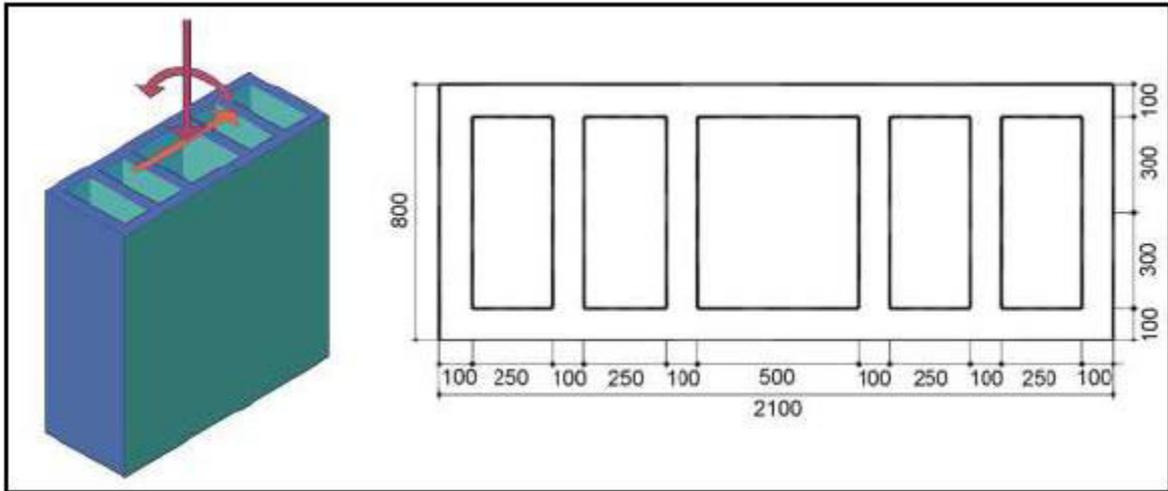


Figure 5: Foundation Concept

1.8. SUPERSTRUCTURE

Superstructure comprises of a steel deck with a length of approximately 1.379 m, 11 steel piers and an abutment made of reinforced concrete. 32,000 tons of steel used in superstructure. The deck section is a twin box orthotropic steel structure continuous for the entire length of the bridge. The two box sections are linked by a series of transverse steel beams which are spaced at 4 m.

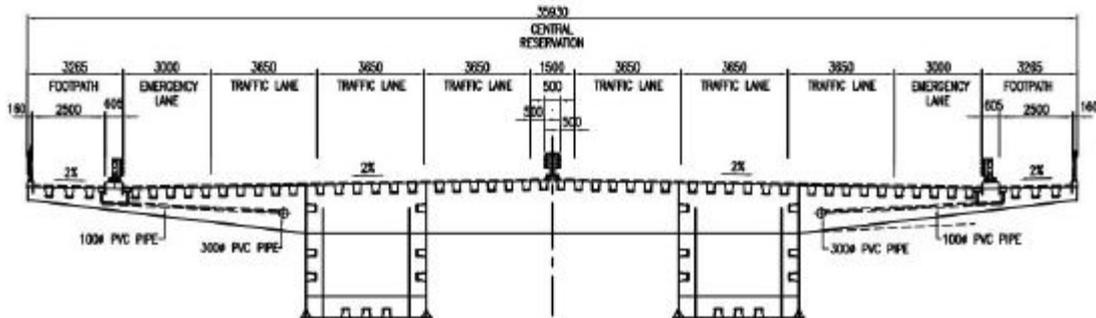


Figure 6: Deck cross-section

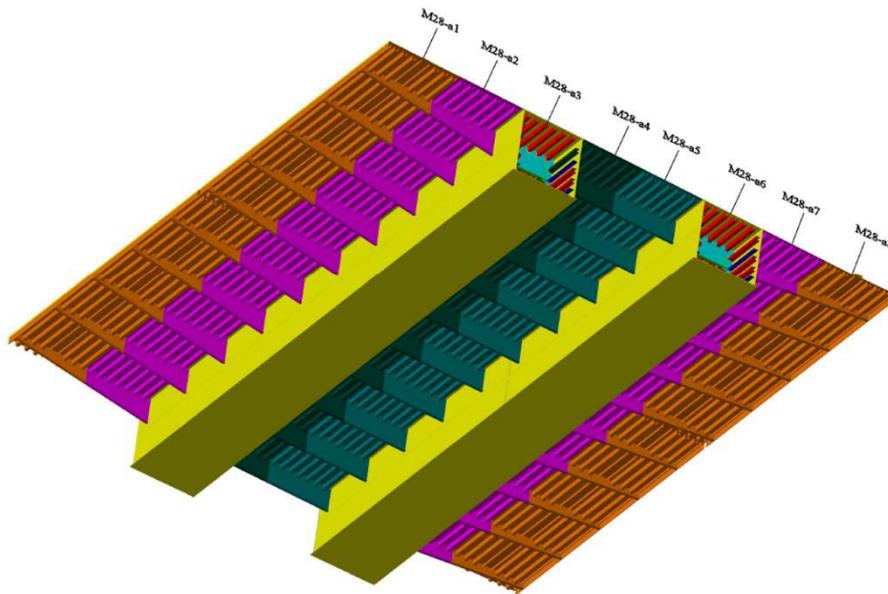


Figure 7: Deck

Piers are flexible steel box (4 m X 4 m) columns. The reason of the selection of the pier structure type and shape is to reduce mass and decrease the structural stiffness which results in a period shift. An increased structural period generally results in a reduction of acceleration. Total weight of piers is 7000 tons.

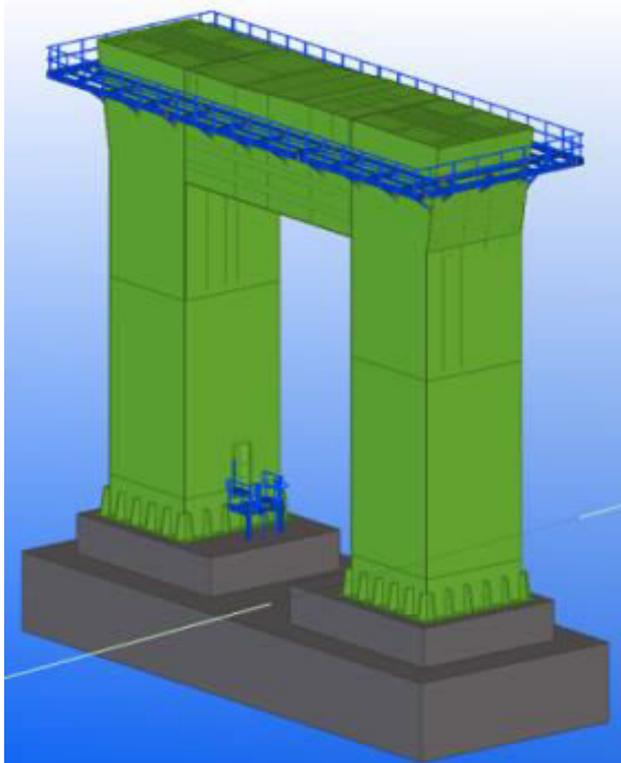


Figure 8 :Piers

All enclosed spaces such as the inside of the piers and cap beam as well as the two boxes of the superstructure are protected against corrosion primarily by dehumidification system.

Due to the fact that this bridge is located in a highly seismic area, with the added complication of a potential fault rupture zone traversing the alignment of the bridge it was required to come up with a special seismic isolation solution for this project in order to ensure that this structure will withstand the specified EQ. The isolation system chosen for this bridge had to fulfill several critical conditions one being the potential large displacement as a result of fault rupture and the second being to ensure and guarantee adequate isolation of the superstructure, to ensure that it performs in accordance with the clients seismic performance requirements. The isolation system that fulfilled all of the requirements essentially consists of LRB bearings as the main vertical load bearing members, in

conjunction with a finely tuned damper system that effectively isolates the superstructure from the substructure during an extreme seismic event, at the same time dissipating large amounts of energy, which is essential for the survivability of this structure.

1.9. PAVEMENT

The area of the main carriageway of South Approach Viaduct is approximately 40,600 square meters. Asphalt pavement built up in two layers comprising a wearing surface stone mastic asphalt top layer and a mastic asphalt layer over waterproofing system on steel decks. It is planned to remove the Stone Mastic Asphalt wearing surface in surface damages without touching the Mastic Asphalt Layer and Waterproofing Layer.



Figure 9: Waterproofing of deck

Wearing course, $t = 30$ mm
Intermediate layer, $t = 28$ mm
Water proofing, $t = 2-4$ mm
Primer

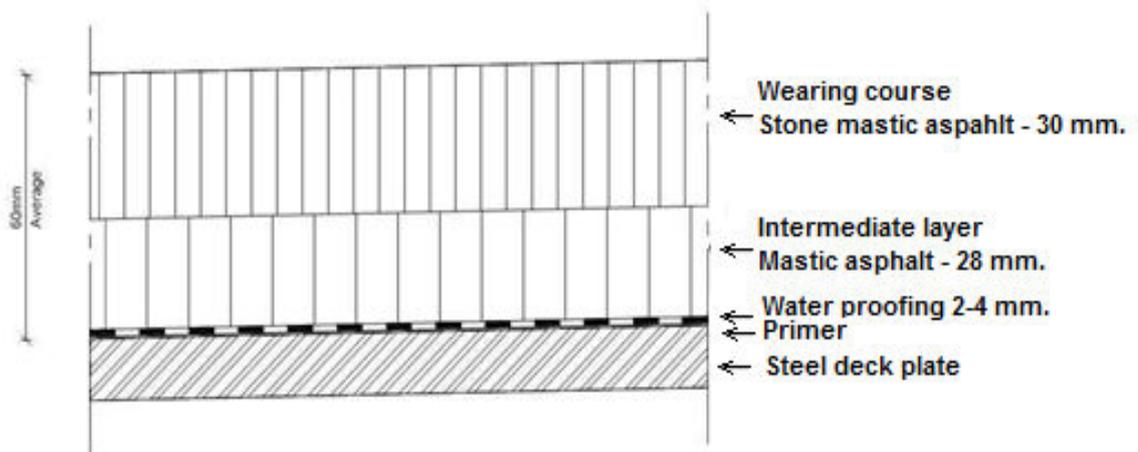


Figure 10: Typical pavement section

1.10.ACCESSORIES

The inspection walkway is protected with anti-skid waterproofing layer and has hot dip galvanized steel barriers. Main reason of selection of the coating system is providing best conditions technically and environmentally on the viaduct walkways. Regarding the specifications, coating system complies with ISO-12944 C5I/M High standard to protect steel surfaces against corrosion. The coating system has its unique properties to provide corrosion resistance according to ISO standard and anti-skid properties. Priority of the system is corrosion protection which is provided by the system contains Zinga and Alufer N. Then Zingacolor and Zinga MixFloor application provides anti-skid feature of the walkways.

Wire type traffic barriers mounted on galvanized steel posts bolted to steel deck. Swivel joint expansion joints (DS1200 and DS880), LRB bearings (with capacity upto 42 MN each), longitudinal and transverse seismic dampers (with stroke of up to 1,175 mm) are installed for isolation.



Figure 11: Expansion joint, seismic damper and bearing

1.11.ELECTRO-MECHANICAL INSTALLATIONS

South Approach Viaduct has following electro-mechanical installations:

- Power supply system
- CCTV system
- Highway lighting system
- Architectural lighting system
- Access control system
- Fire alarm system
- Fire fighting system
- Dehumidification system
- SOS telephones and communication system



Figure 11:Electro-Mechanical systems

The control and monitoring of the technical installations on the bridge are carried out from two redundant control rooms located at the following facilities:

- Main Control Room in the Main Control Building
- Slave Control Room in South Substation Building

These rooms are center of SCADA to control and monitor all bridge structural and operational functions.

1.12. DEHUMIDIFICATION SYSTEM

Corrosion of structural steel elements are main factors adversely affecting the condition of the steel bridges. All closed parts of South Approach Viaduct are equipped with dehumidification system, monitored and controlled from bridge control center. Dehumidification system introduces dry air into the internal parts of bridge to remove moisture and to maintain a relative humidity below 40% level to suppress corrosion.

1.13. DESIGN SPECIFICATION

The main steel structural design carried out in accordance with AASHTO LRFD Bridge Design Specifications, 6th Edition – 2012.

1.14. DESIGN LOADS

Permanent Loads:

- (a) dead load (DL)
- (b) superimposed dead load (SDL)
- (c) horizontal earth pressure (EH)
- (d) creep and shrinkage (CR+SH)

Transient Loads:

- (a) vehicular live load (LL)
- (b) vehicular dynamic load allowance (IM)
- (c) vehicular braking load (BR)
- (d) vehicular centrifugal load (CE)
- (e) live load surcharge (LS)
- (f) pedestrian live load (PL)
- (g) special vehicles (LLs)
- (h) wind load on structure (WS)
- (i) wind on live load (WL)
- (j) force effect due to uniform temperature (TU)
- (k) force effect due to gradient temperature (TG)
- (l) force effect due to settlement (SE)
- (m) earthquake load (EQ)

Design truck : (H30-S24)

The design tandem : A pair of 110 kN axles spaced 1.20m apart.

The design lane load : A load of 15.0 kN/m uniformly distributed in the longitudinal direction. Transversely, the design lane load shall be assumed to be uniformly distributed over a 3.00 m width.

Abnormal highway loading : "Special vehicles" with reference to EN 1991-2. Section 4.3.4. And the design live load intensity of 81.7 kN/m in UDL system.

Abnormal load Type A : Unlimited convoy of two tracked crawler military tank weighing 1335kN.

Abnormal load Type B : Unlimited convoy of vehicles weighing 1512kN and having five axles.

Abnormal load Type C : Single vehicle weighing 1800 kN and having four axles.

The wind pressure : Specified in AASHTO LRFD was assumed to be caused by a base design wind velocity, V_B , of 160 km/hr.

Seismic Loading: Analysis of extreme and lower risk design earthquake events, with a final check on the bridge design for a third more extreme seismic event. The bridge is designed to provide the specified levels of seismic performance described below. It shall be designed to resist three levels of earthquake:

- A Functional Evaluation Earthquake (FEE), with a 50% probability of occurrence in the 100-year design life specified for the bridge (return period of ~150 years).
- A Safety Evaluation Earthquake (SEE), with a 10% probability of occurrence in the 100-year design life specified for the bridge (return period of ~1,000 years).
- A No Collapse Earthquake (NCE), with a 4% probability of occurrence in the 100-year design life specified for the bridge (return period of ~2,475 years).

KAPSAMDA BULUNAN SİSTEM VE ALANLAR	İlgili Form	Yılı																							
		(Deneyim yılı)	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037		
Aktüer																									
Yüksek basınç tesisleri, Du	İVİM-001																								
Çelik Ayaklar, Du	İVİM-002																								
Çelik Ayaklar, E	İVİM-003																								
Muayene																									
Tablolar, Du	İVİM-009																								
Tablolar, E	İVİM-010																								
Masa	İVİM-013																								
Genleşme Derzleri	İVİM-014		0	0	0	0																			
Yüzey kaplaması, yol ve seride yayıyolu	İVİM-015																								
Yardımcı Yapılar																									
Feritler, Derzler, Arac Paraseti, Yeni Derzler ve Bilezik Kalınları (E ve Du)	İVİM-016																								
Kapılar, Penceler, Tirmenler ve Basamaklı Merdivenler	İVİM-017																								
Aydınlatma direkleri, (diğer) Şarjörleri ve diğer Dekoratif parçalar	İVİM-018																								
Mekanik & elektrik tesisatı																									
Oranaj sistemi	İVİM-019																								
Harici aydınlatma	İVİM-020																								
Tesisat (kaldırma, trafo, dahil aydınlatma)	İVİM-021																								
Yıldırım koruma ve topraklama	İVİM-022																								
Tablolar ve Çelik Ayak Nem Alma Sistemi	İVİM-032																								
Hidrolik sistemler	İVİM-033																								
Diğerler																									
Genel ölçüm (E-3 yada E-4 ile, sonra 2-5-10 yıl ara ile)	İVİM-037		0	0	0	0																			
DM : Büyük Muayene Ö : Ölçüm																									
HAZIRLAYAN :		ONAYLAYAN :																							

Table 12: Principal inspection plan

Damages identified by Principle Inspection are documented according to the following principles with categorization of inspection results into 4 damage levels.

Damage Level	Damage	Documentation
0	No damage (not visible within arms length)	Condition may be noted as a general observation.
1	Minor damage. Damage is stable.	Condition is noted and sample picture taken for record
2	Moderate damage. Damage may develop into damage level 3 before next Principle Inspection.	Condition is noted and damage described. Sample picture of damage and cause of damage. Repair may be considered if economical feasible.
3	Serious damage. Damage has or will before next Principle Inspection, develop into failure or loss of function.	Condition is noted and damage described. Sample picture of damage and cause of damage. All damages are documented in detail as a basis for ordering Special Inspection and repair or replacement.

Table 13 : Damage levels for inspection

2.2. ACCESS FOR INSPECTION AND MAINTENANCE

Access for inspection and maintenance were taken into consideration during design phase. There is an inspection walkway on both side of roadway in each direction. Doors, hatches and stairs are provided to reach to deck and piers whereas mobile underdeck platform is used to access to underdeck and outside of piers.



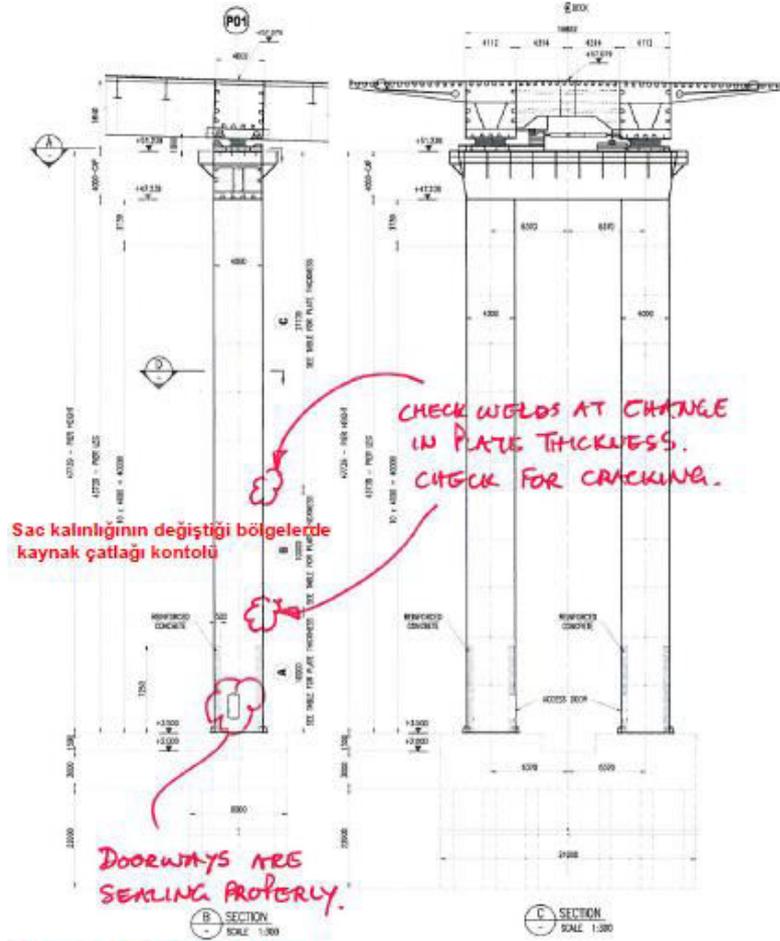
Figure 12: Mobile underdeck gantry



Figure 13: inspection walkway (fixing of bird protection on pedestrian barrier)

2.3. VULNERABLE POINTS

The designer advised following points to check closely within the operation and maintenance manual:



Kapı girişleri sızdırmazlık kontrolü

Figure 14 : Guide for inspection of piers

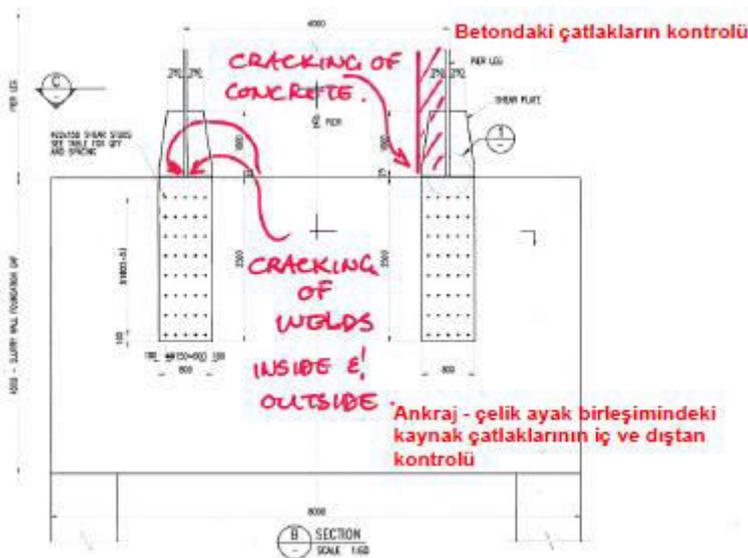


Figure 15: Guide for inspection of foundations

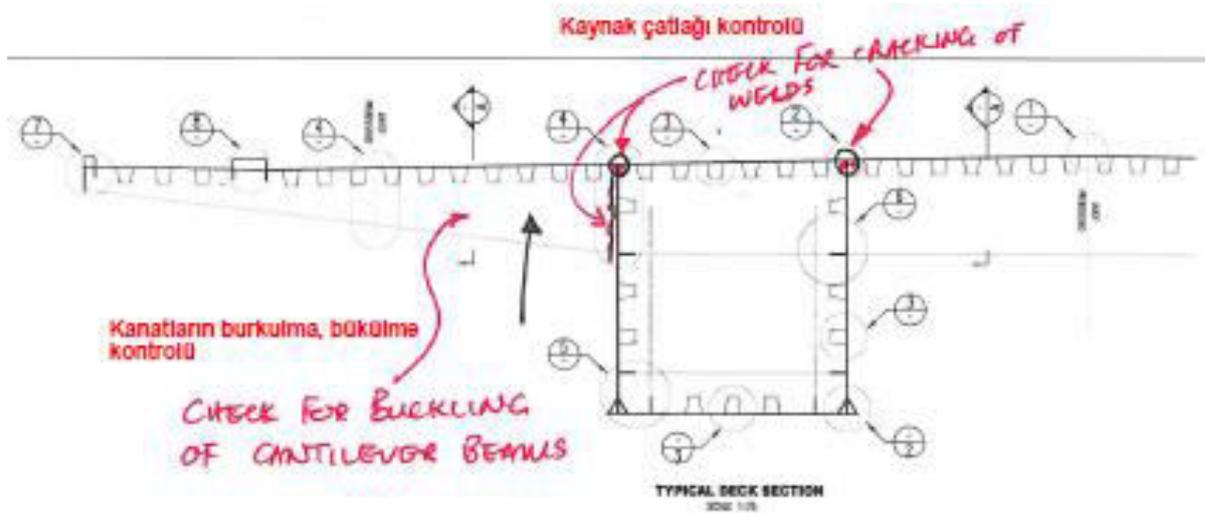


Figure 18: Guide for inspection of deck welds

3. DEFECTS

The bridge is designed for 100 years and material are selected to fulfill this requirement. Since the bridge is new and well maintained only minor defects are observed during routine inspection. The biggest defect observed yet from opening was the defected area of asphalt pavement at km: 7+660 in Izmir direction.

3.1. ASFALT DEFECT AT KM: 7+660

Asphalt defect was observed on 28.02.2018, and cold patch was applied immediately to ensure traffic safety. Permanent repair was postponed to a suitable day.



Figure 19: Defect in asphalt



Figure 20: Cold patch as temporary repair

Asphalt defect was permanently repaired 02.04.2018 and following sequence is applied as per repair procedure:

- Removal of loose asphalt portion
- Removal of existing waterproofing layers
- Sand blasting SA 2 ½ of steel deck
- Application of new waterproofing layers
- Application of mastic asphalt



Figure 21: Removal of existing waterproofing layers and sand blasting



Figure 22: Primer



Figure 23: 1st layer waterproofing membrane



Figure 24: 2nd layer waterproofing membrane

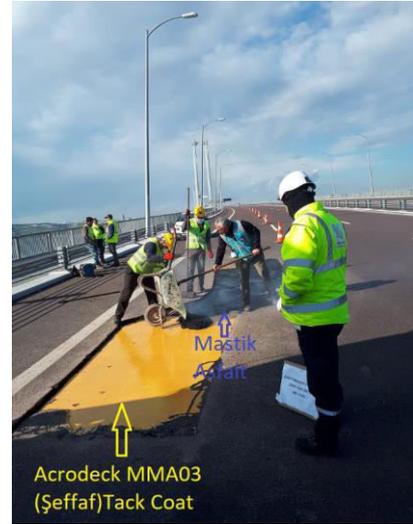


Figure 25: tack coat



Figure 26: Laying of mastic asphalt



Figure 27: completed repair

4. POTENTIAL FAILURE MODE OF THE BRIDGE

The bridge is designed for 100 years to withstand design loads and even not collapse in earthquake of NCE with a 4% probability of occurrence in the 100-year design life specified for the bridge (return period of ~2,475 years). The bridge is continuously monitored with CCTV and SCADA systems plus regularly inspected by GIBB maintenance teams. The data from SHMS (Structural Health Monitoring System), SCADA system and other sub-control systems (such as dehumidification system) are used to make assessment and optimize the required maintenance.

5. MATERIALS OF THE BRIDGE

Special performance based C45/55 concrete comprising 380 kg/m³ slag cement, W/C ratio 0,38 and chloride migration coefficient at 28 days is smaller than 3×10^{-12} m²/s is used. C50 prefabricated concrete spacers are used in concrete covers.

S355 J2+N quality structural steel used in piers and decks and externally coated with Zinga zinc rich paint to serve minimum 35 years without any major repair. The surface of the decks are painted with zinc rich epoxy as first coat, polyamide cured epoxy or fast dry zinc phosphate epoxy used as an intermediate coat and aliphatic polyurethane paint to be used as final coat which has been specified as follows;

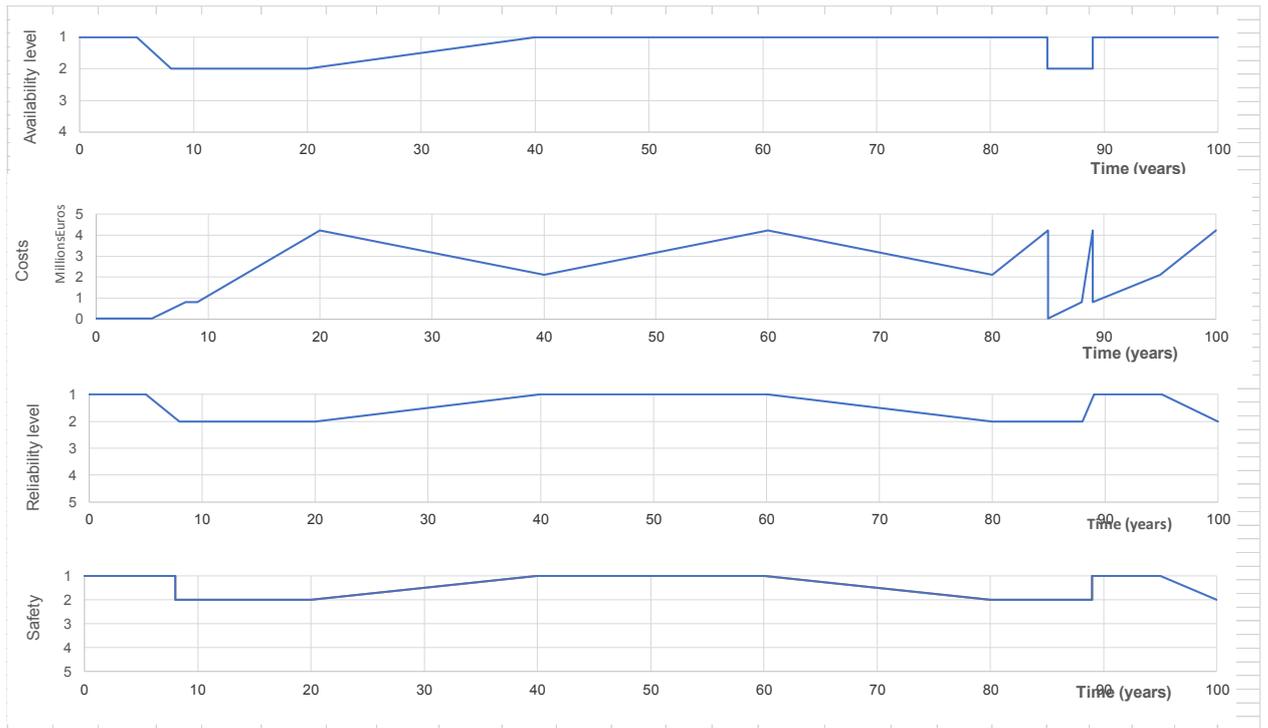
- 1x60 micron Primer : Zinga
- 1x80 micron Intermediate : Alufer N
- 1x60 micron Final : Zingaceram PU

6. PERFORMANCE APPROACH

6.1. PREVENTATIVE APPROACH

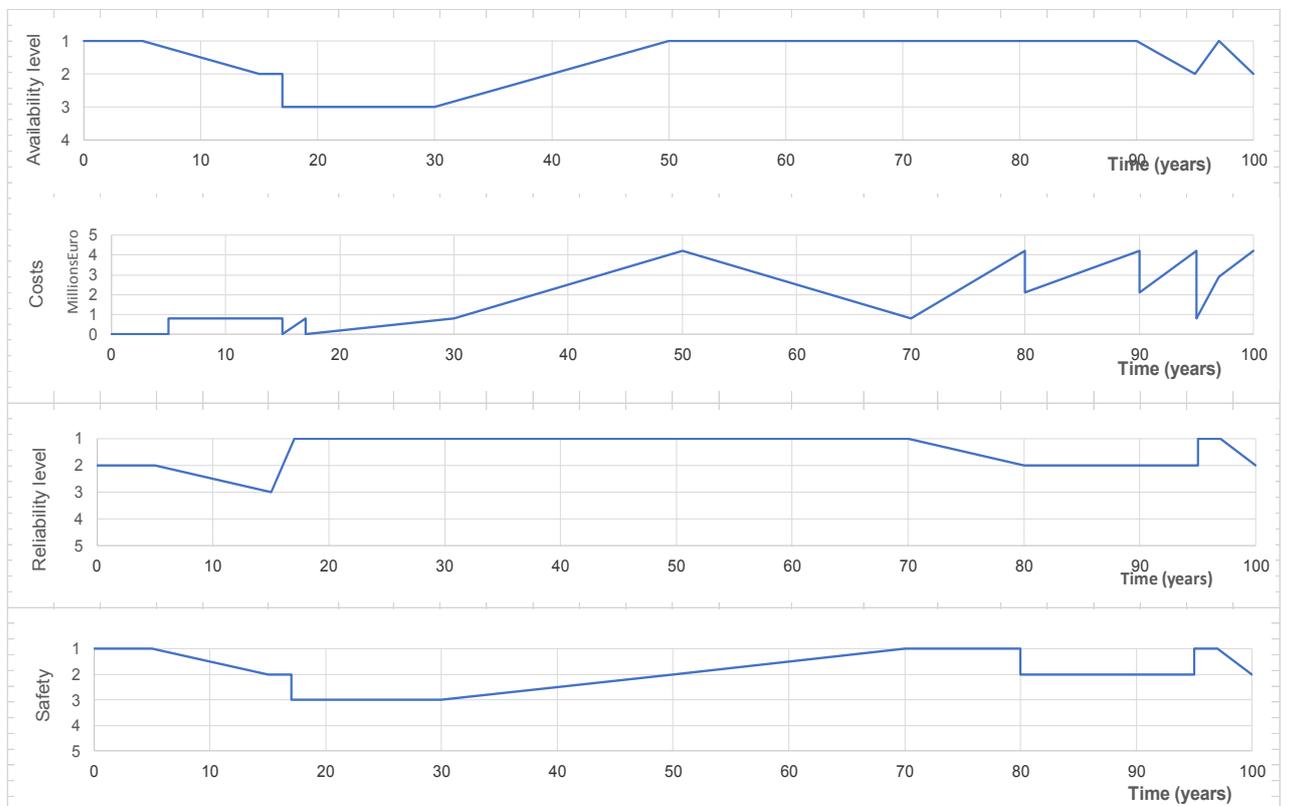
As a policy of the Concessionaire company, routine inspections will be carried out regularly by bridge control team, sufficient spare part shall be kept in stock and any observed defect shall be immediately repaired to ensure durability of the South Approach Viaduct that is a part of Osmangazi Bridge crossing for uninterrupted and safe traffic flow of Gebze-Izmir Motorway. The wearing surface asphalt pavement replacement assumed to be after fifteen years. Planned maintenance intervals for replacement of major maintenance items are selected as below:

Surfacing replacement	: 25 years
Structural bearings	: 25 – 50 years
Expansion joints	: 25 years
Dampers	: 25 years
Concrete surface repairs	: Nil – 100 years
Structural steelwork minor	: 15 years
Structural steelwork paint	: 35 years
Lighting columns (structure)	: 30 years
Sign gantries (structure)	: 30 years

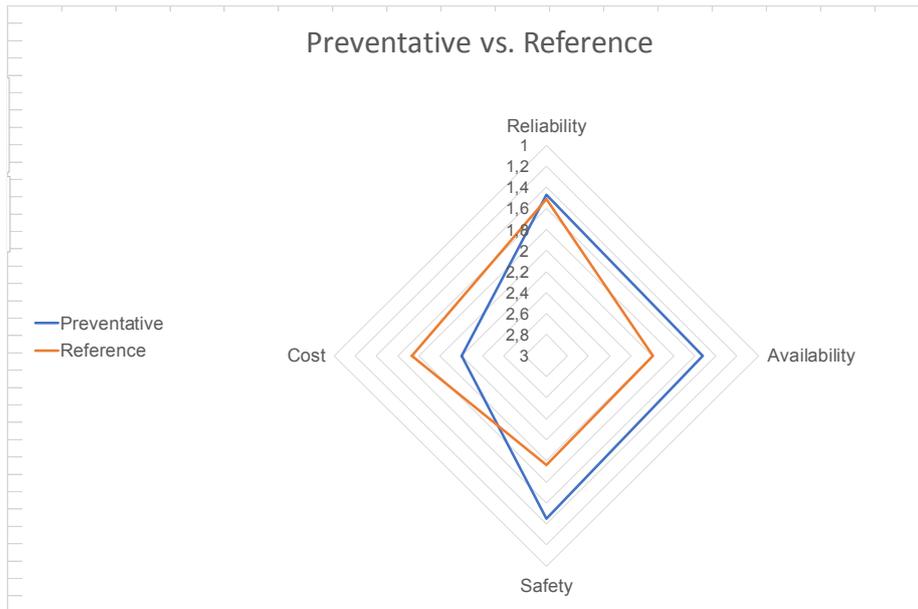


6.2. REFERANCE APPROACH

Although this approach is not applicable to management policy of operator, it is studied as to perform the minor repairs and postpone the significant repairs.



Comparison of two approaches is shown in following spider diagram:



Preventative approach is more appropriate for South Approach Viaduct.

7. CONCLUSION

With challenging construction materials (like use of protective coating of zinc rich Zinga paint instead of classical three-coat paint system) and protective measures (like dehumidification system) South Approach Viaduct will have a longer life and require less maintenance.



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